

Developing 3-D Imaging Sensors

Problems and Technologies

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Outline

- outlook to 3D applications
- time-of-flight measuring technique
- comparing PULSED and SWM approaches
- developing the Photo-demodulator in CMOS
- measurements and conclusions

3-D Imaging

Today's technology is ready to develop photodetectors for the three-dimensional world !!



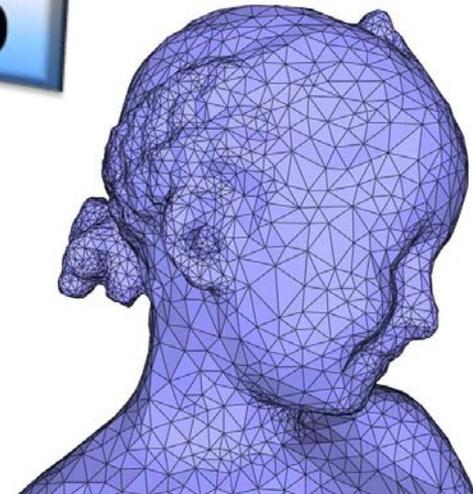
**pixels describe
the intensity
pattern $I(x,y)$**

2D



adding
distance
information

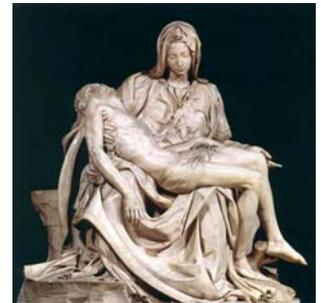
3D



**pixels describe
morphology
 $z(x,y)$**

typical applications

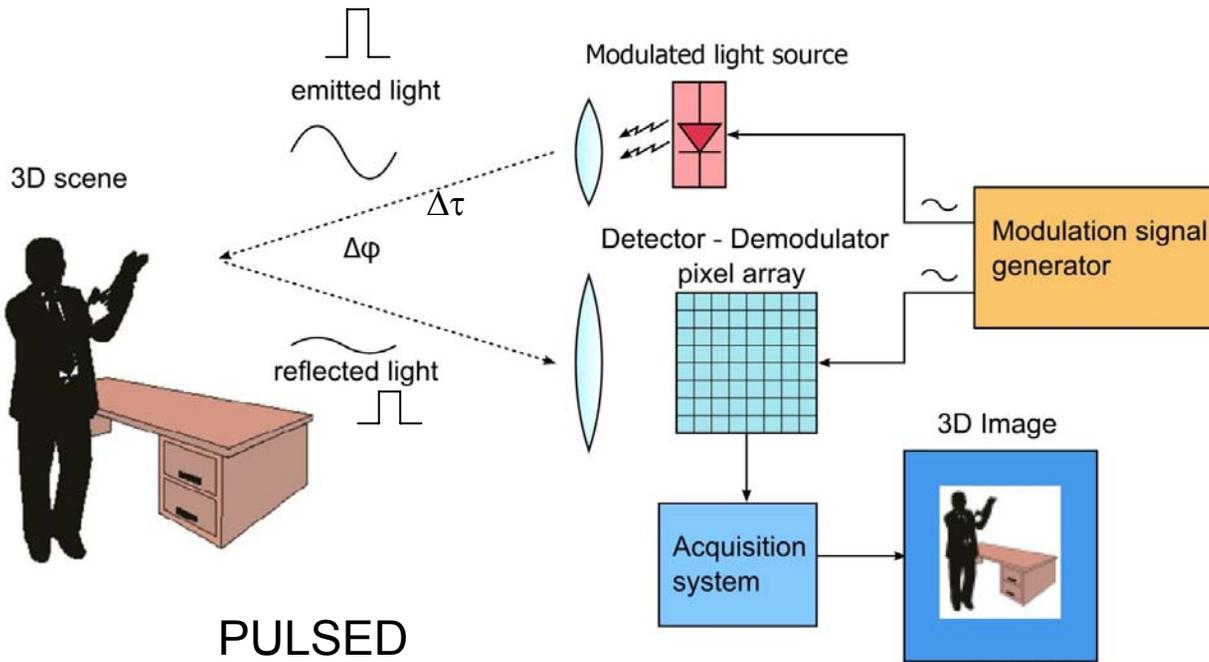
- Homeland security
- Navigation aids
- Virtual reality
- Robotics
- Cultural heritage
- Ambient assisted living



techniques for 3D imaging

- Triangulation
 - bulky, requires scanning short distance
 - medium/low resolution
- Interferometry
 - very high resolution
 - expensive, critical to operate
- **Time-of-flight** (pulsed or SWM) 
 - Compact, may be scannerless
 - Fast acquisition
 - Large distance range
 - Cost-effective 
 - Active (illuminator required) 
 - Ambiguity range limitation

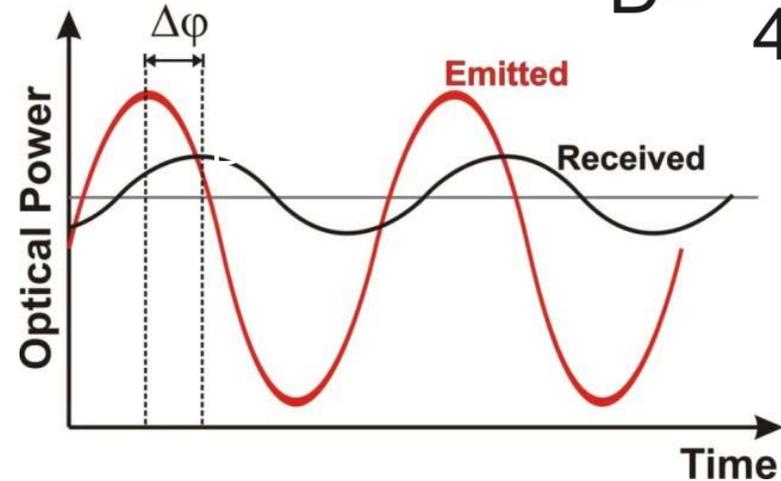
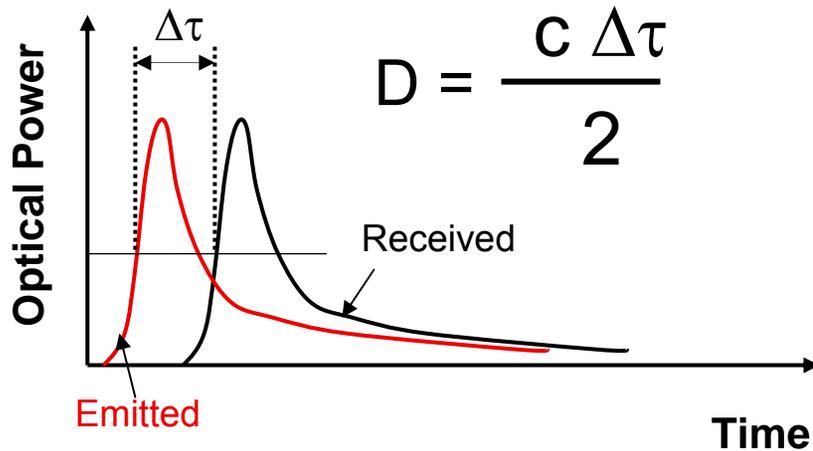
Time-of-Flight rangefinders



PULSED

SW (sine wave)
Modulated

$$D = \frac{c \Delta\phi}{4\pi f_m}$$



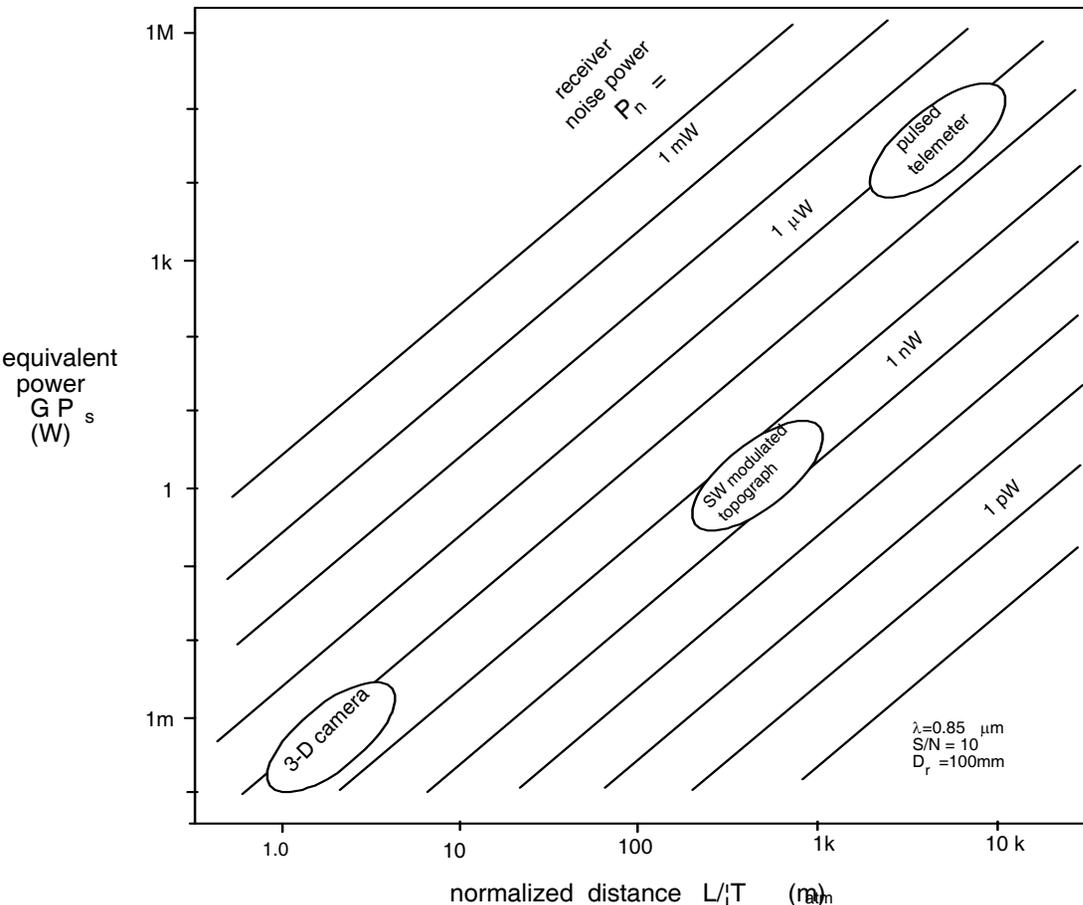
in most applications, to be interesting...

both PULSED and SW 3-D developments should entail:

- integration of time-of-flight pixel on-board technology with the Silicon CMOS industry standard (and ... *low-cost !!*) technology
 - minimum invasiveness (optical power) of the active illumination required
-

analyzing Time-of-Flight rangefinders: pulsed vs SWM

$$GP_s = (S/N) P_n 4L_{eq}^2/D_r^2$$



theoretically equivalent at the quantum limit at equal average power, but PULSED is less sensitive to stray light, has some safety issues and requires more bandwidth to circuits. SW-modulated is short-distance, is about eyesafe, but has range ambiguity to circumvent

other features of PULSED and SW

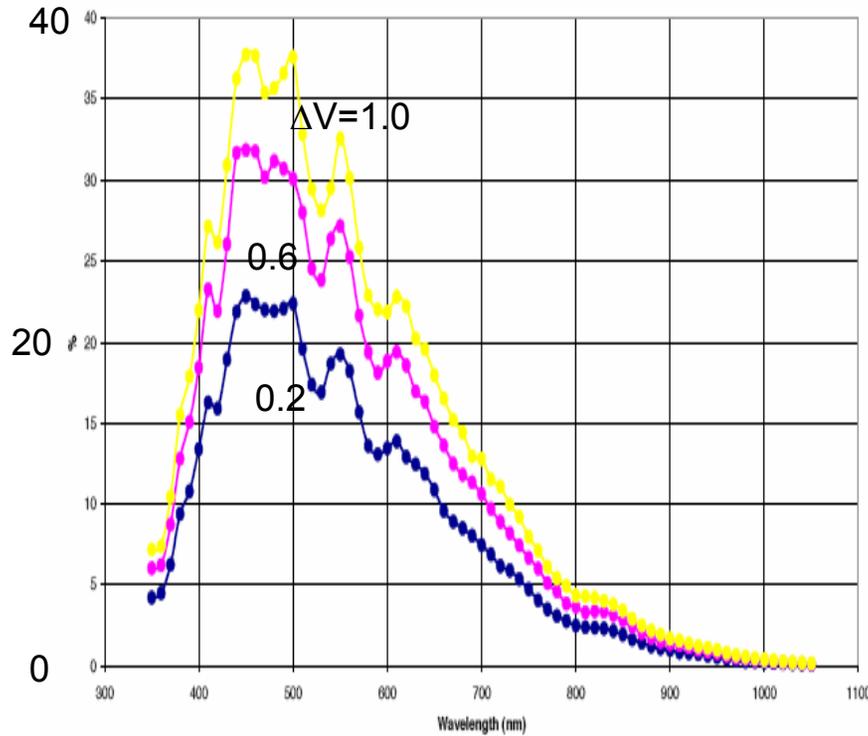
- Pulsed 3-D requires a fast (sub-ns) detector for operation on short distances, and very fast time sorters to measure the ns-range time delay → SPADs and Counters with TAC
- this makes the pixel large and fill-factor low, requiring a lens-array for sensitivity recovery
- SW works on moderate frequency (20 to 100 MHz) for 3-D short range, and by incorporating a demodulator into the detector → circuits are greatly simplified, and fill-factor is high

detour on the PULSED 3-D approach

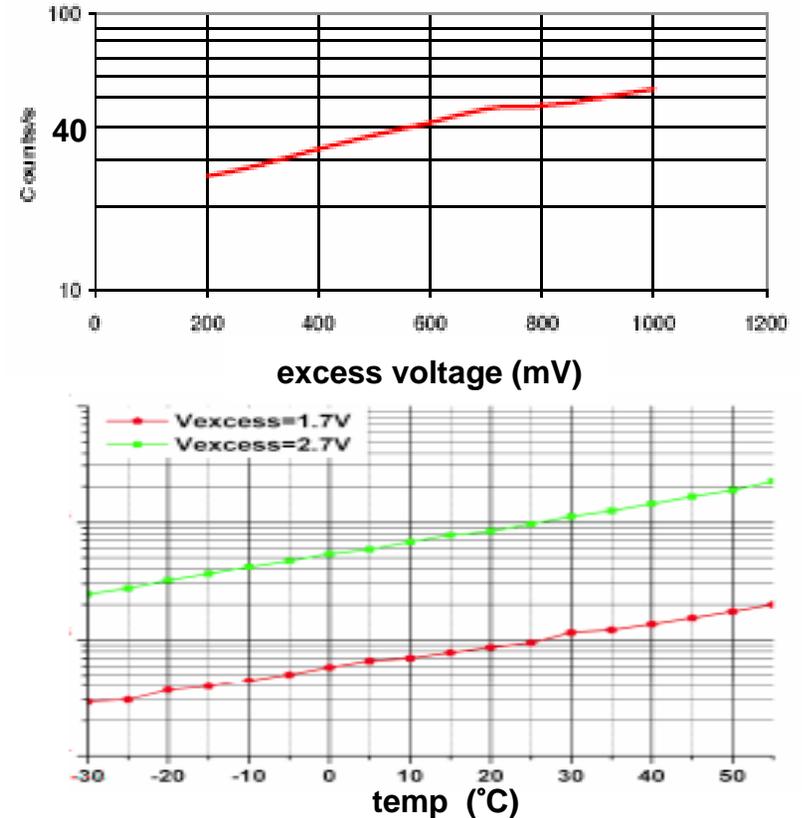
- in 3-D, PULSED is a competitor to SWM but calls for a fast (sub-ns) detector able to resolve the sub-ns propagation times of short-range applications
- the SPAD (Single Photon Avalanche Detector) is the suitable choice of photosensor
- SPAD is compatible to fine CMOS technology
- an *FET-STREP European Program* pursued development of a 120-nm CMOS 3-D and fast spectroscopy imaging (32x32 and 128x160 pixels) device – the *MEGAFRAME* project

CMOS SPAD parameters

a 50 μm active diameter devices has been designed in 120-nm CMOS with good performances of:



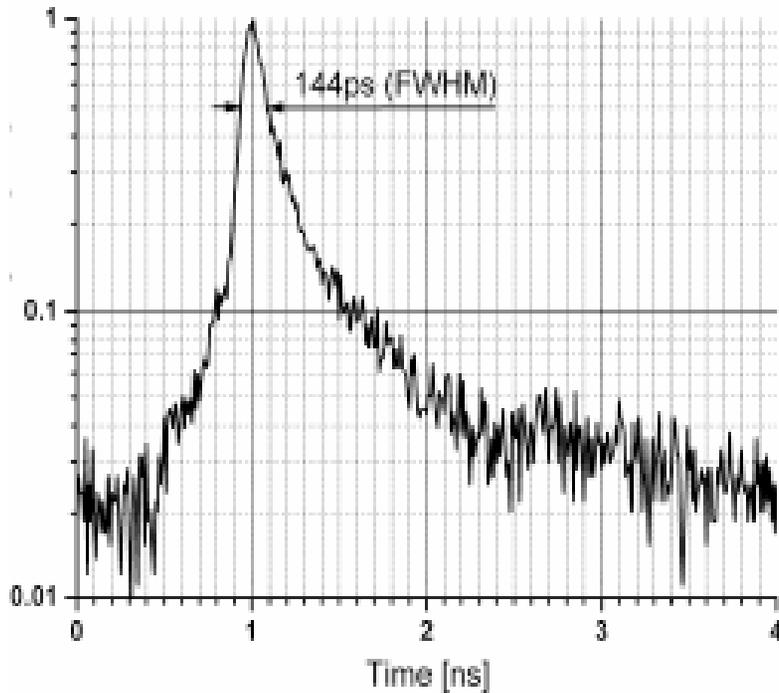
high probability of detection
(35% @ 1-V overdrive)



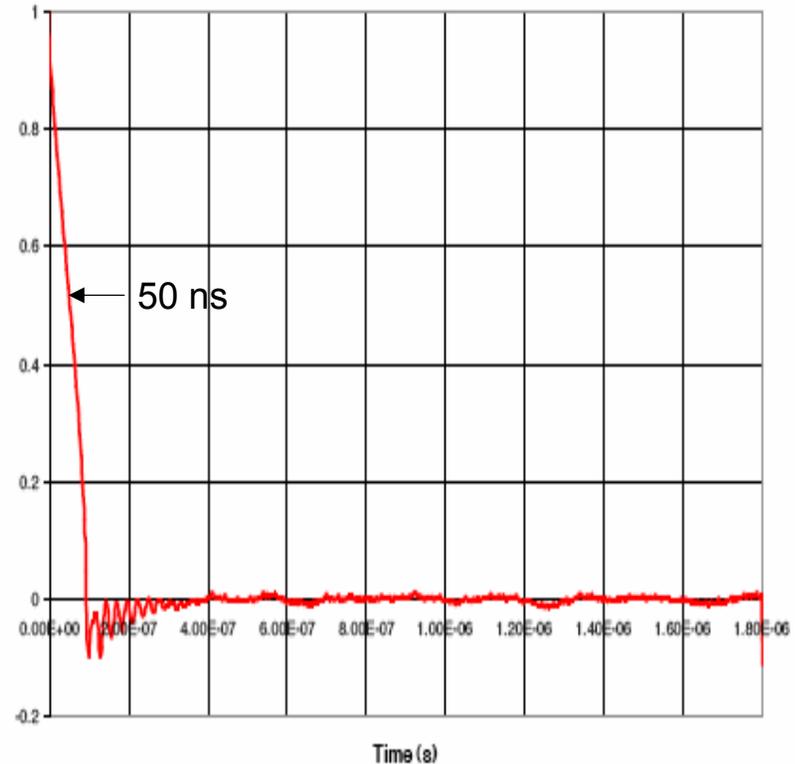
low dark counts rate
(40 Hz for a 6- μm dia.)

CMOS SPAD parameters II

and, not less important:



sub-ns time resolution
(61 ps rms)



low afterpulsing
(negligible @ $T_{ho} > 200\text{ns}$)

On-board pixel processing

processing circuits implemented by CMOS technology in a 50- μm dia. pixel area around the 6- μm SPAD:

- active quenching
- preamplifier
- TAC
- comparator
- 8-bit memory

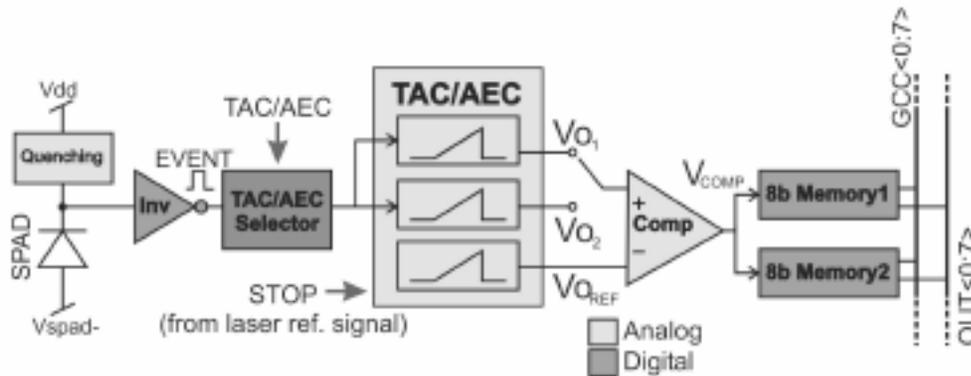


Figure 1. Pixel block diagram.

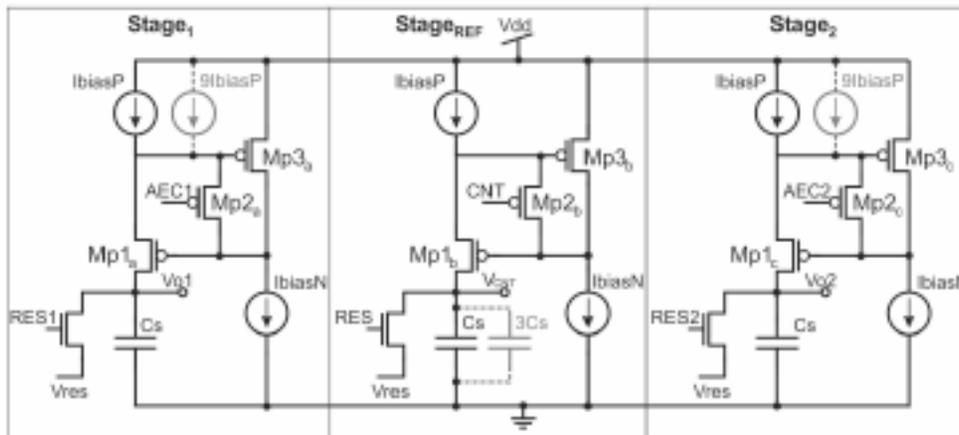
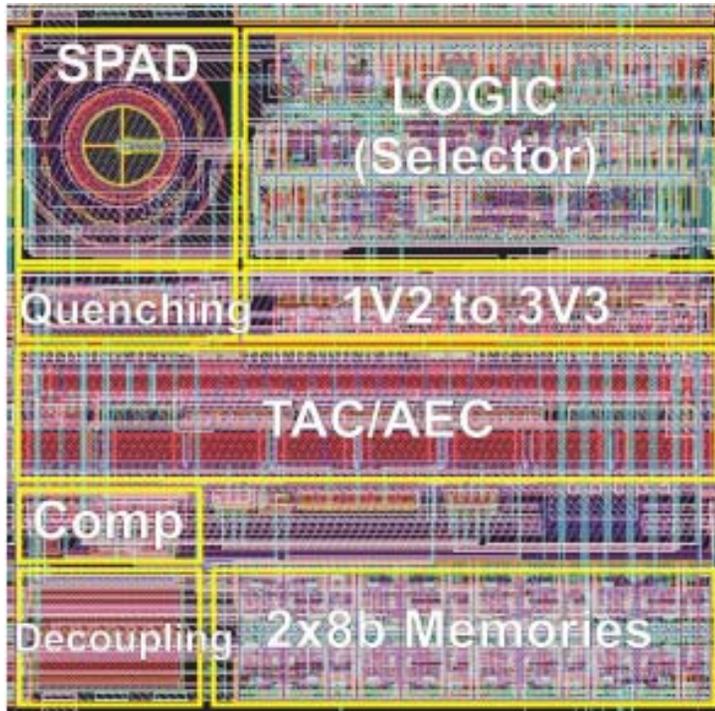


Figure 2. Circuit schematic of the TAC/AEC stage.

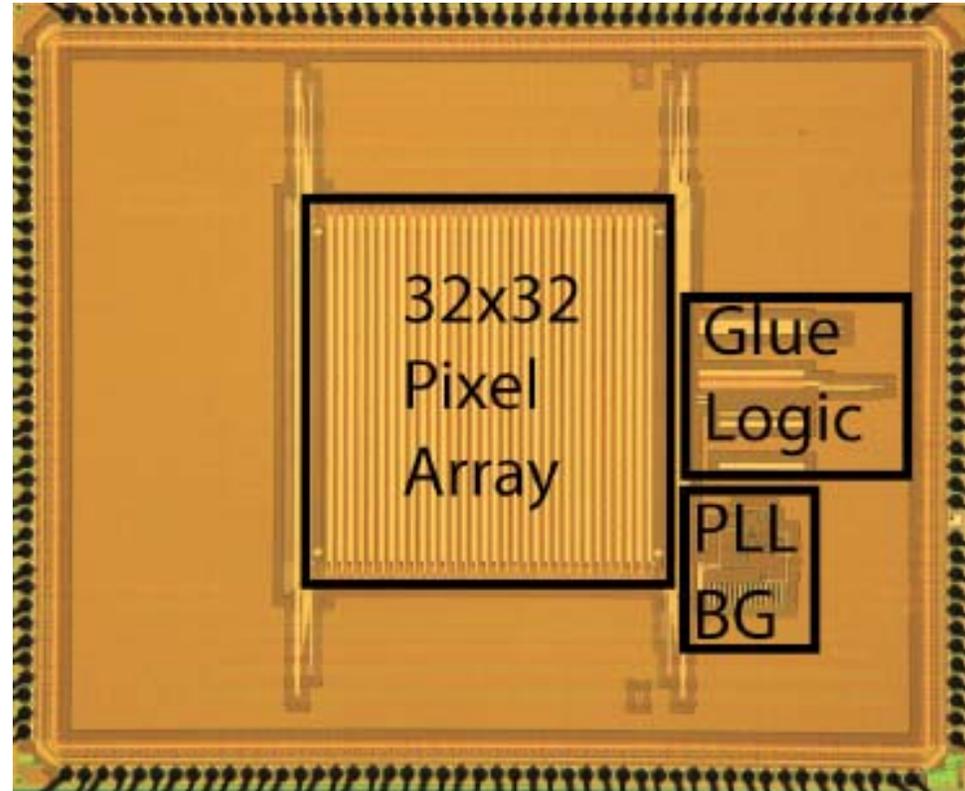
the CMOS SPAD pixel...

the pixel, 50- μm
by side



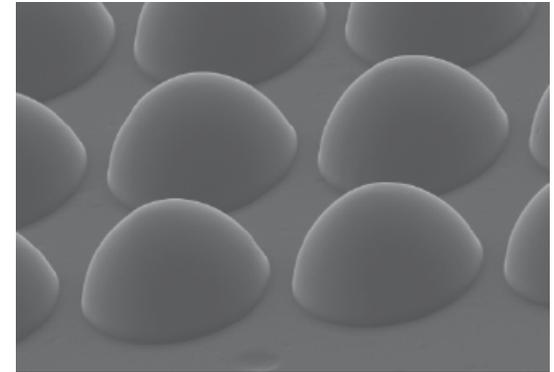
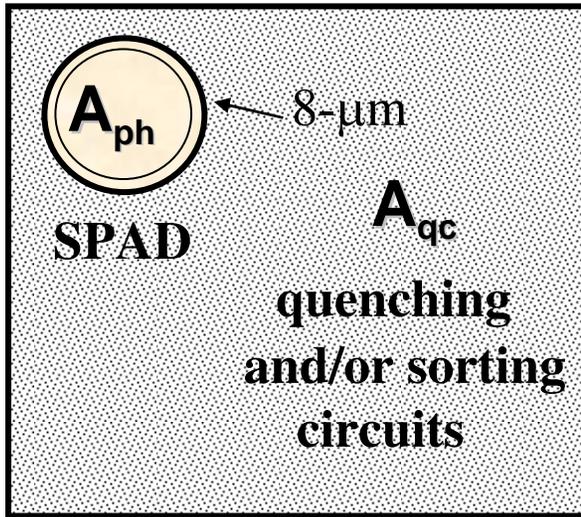
$$FF = A_{ph} / (A_{qc} + A_{ph})$$

(~ 0.02 in example above)



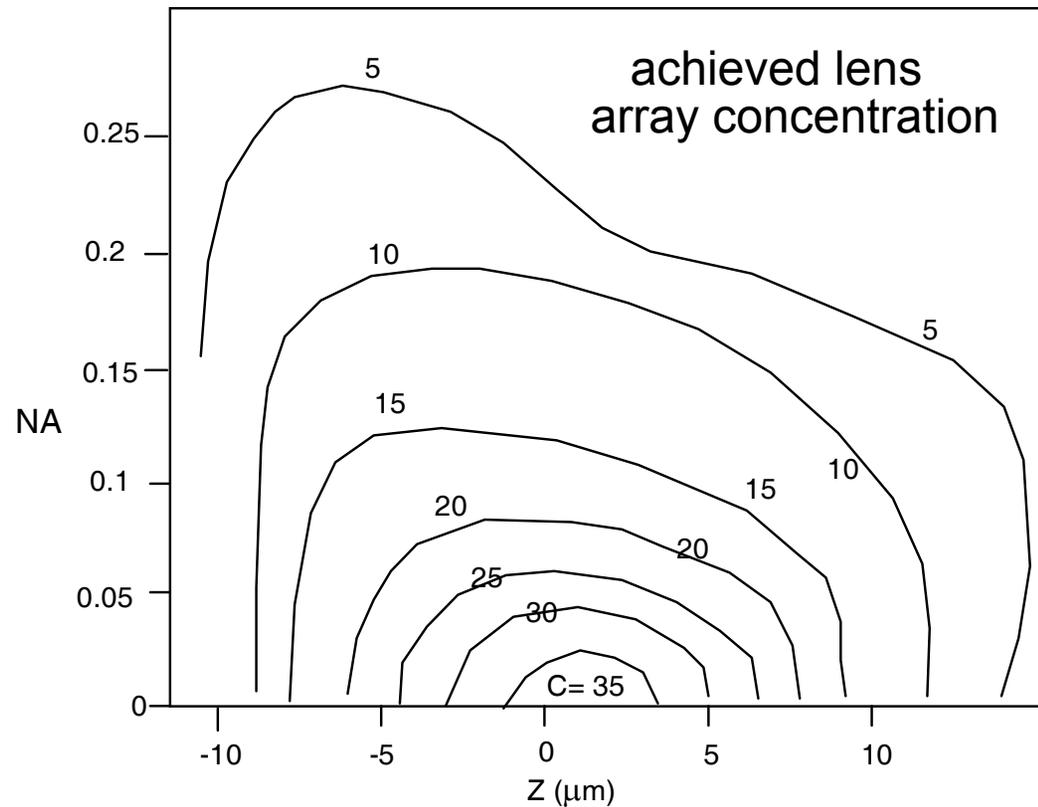
...and the 32x32 array
chip, 4-mm by side

fill-factor recovery in SPAD

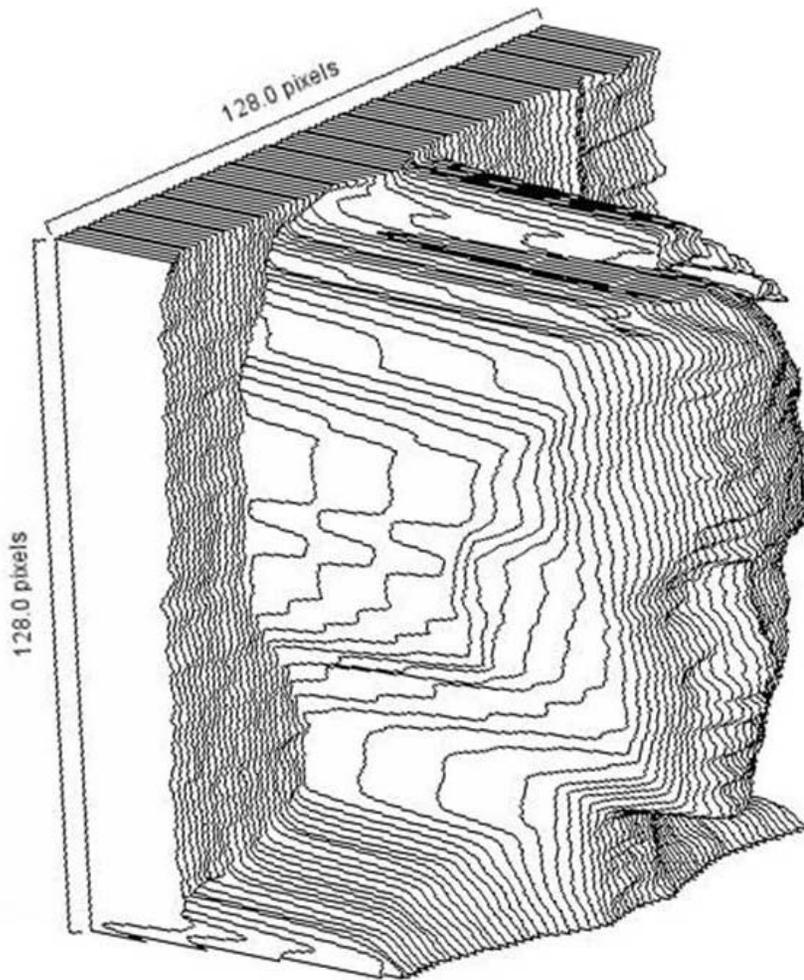


$$FF = A_{ph} / (A_{qc} + A_{ph})$$

 ~ 0.02 in example above
then we use a $50\text{-}\mu\text{m}$ dia.
lens-array to concentrate
incoming optical power



Example of 3D image pickup with the 32x32 SPAD array



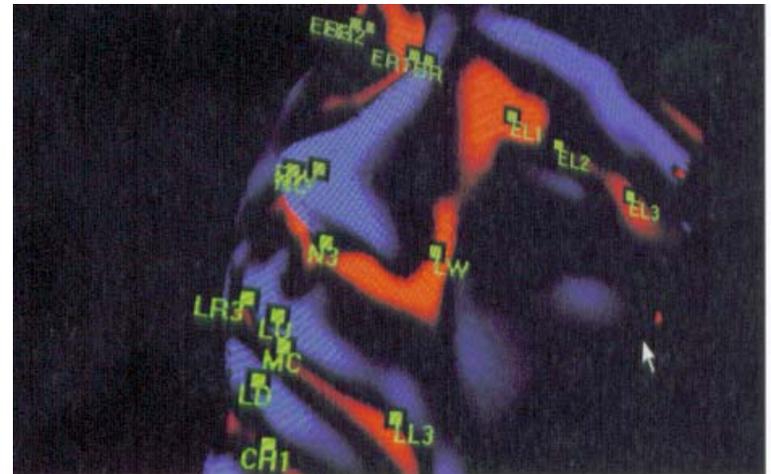
Accuracy:

- 1mm (100 frames)

Frame rate:

- 1Hz

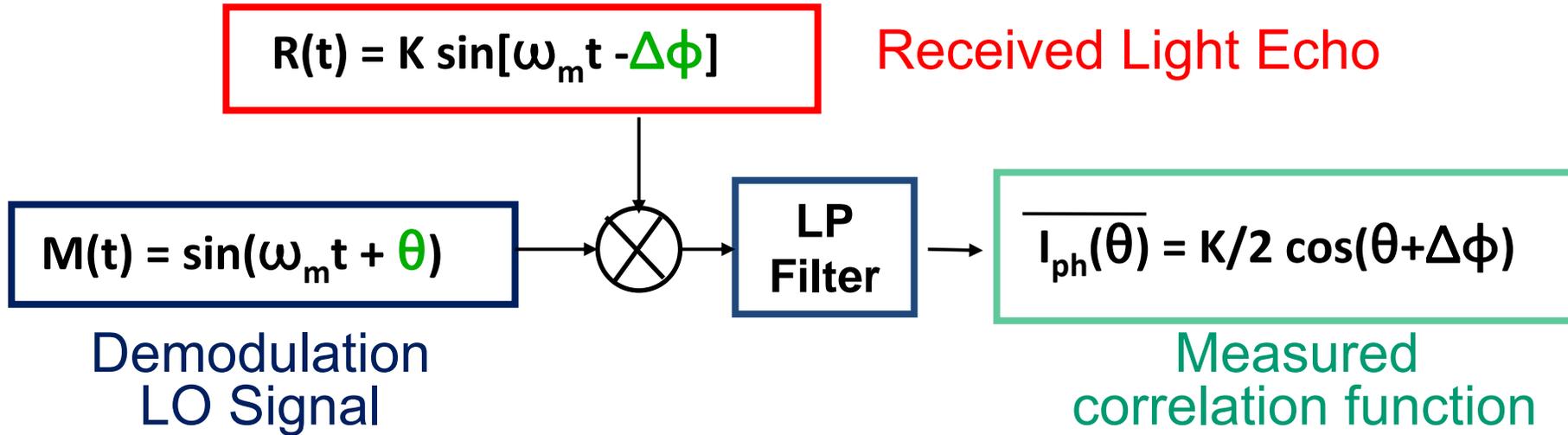
8-bit digital output



going back to SW-modulated...

- the SWM is attractive for 3-D if we can simplify data analogue processing
 - then, we are asked to devise a high-efficiency photodetector, working with shallow epi-layer of a CMOS, low cost, standard industry process.
 - the answer has been a specially designed, CMOS-compatible, high FF, photodetector demodulator
-

principle of SWM telemeter



recovery of phase $\Delta\phi$ amenable to CMOS integration of the pixel: the detected demodulation signal $I_{ph}(t)$ is sampled on 4-phases θ periods of the local oscillator $M(t)$ so as to supply $I_1 = I_{ph}(\theta=0^\circ)$, $I_2 = I_{ph}(\theta=90^\circ)$, $I_3 = I_{ph}(\theta=180^\circ)$, $I_4 = I_{ph}(\theta=270^\circ)$, then we compute

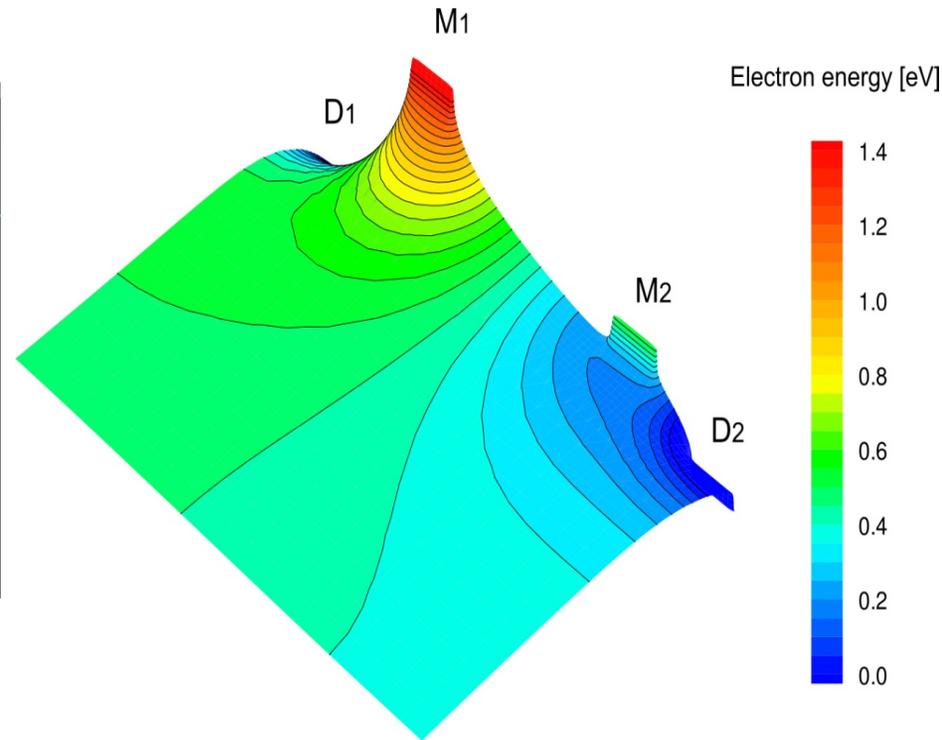
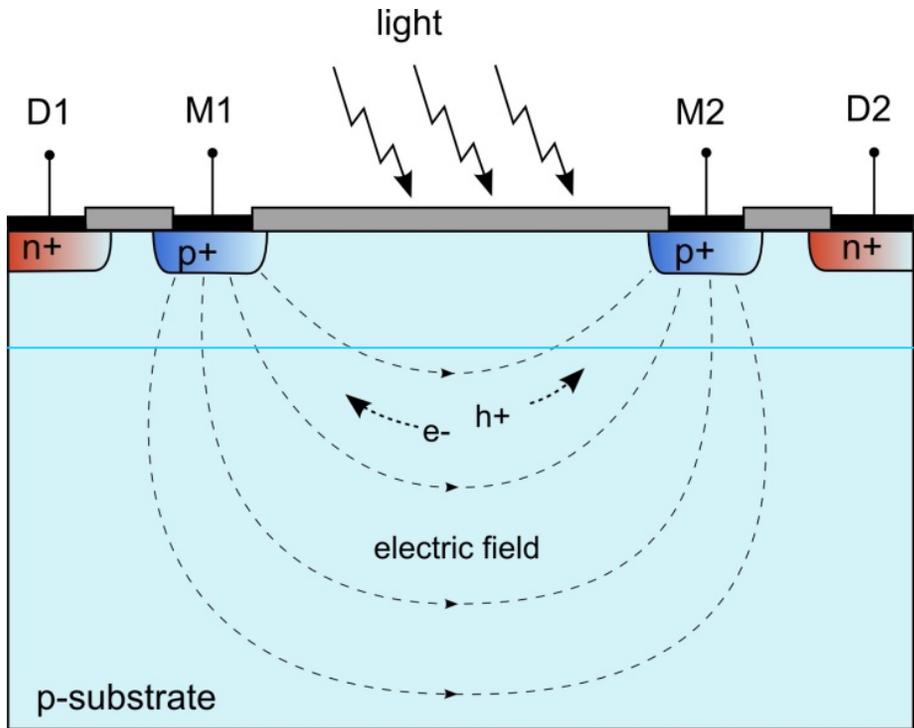
$$\Delta\phi = \arctan\left(\frac{I_4 - I_2}{I_3 - I_1}\right)$$

let's now have a look at

sensor architecture

- design of a new photo-demodulator
 - pixel design
 - array architecture
-

PDD, the Photo-Demodulator Detector

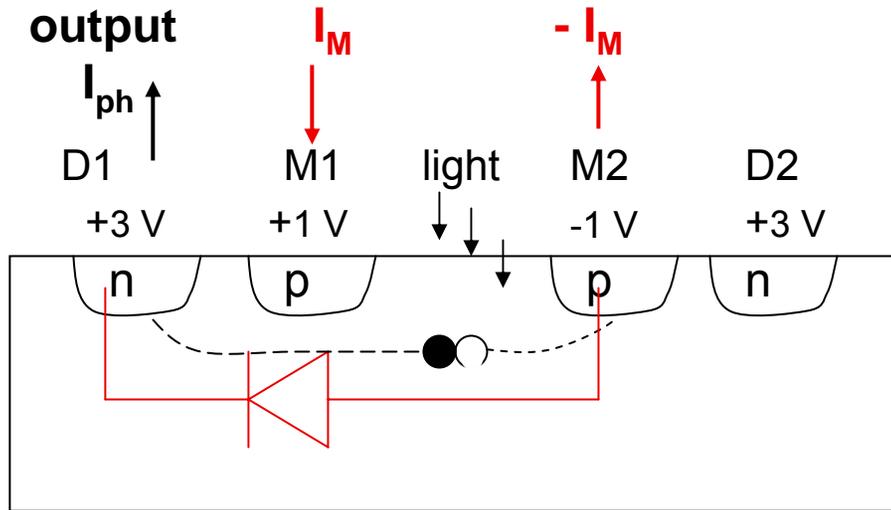


M1, M2: modulation electrodes

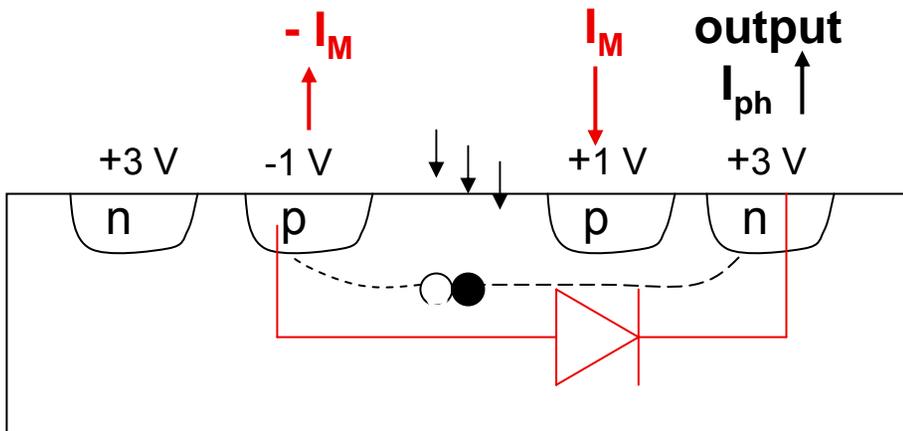
D1, D2: collection electrodes

first reported by: Van Nieuwenhove, et al., Proc. Symp. LEOS Benelux Chapter, 229-32 (2005)

more on the PDD



by pulsing a current I_M ($50\mu\text{A}$ typ.) between electrodes M1 and M2, we can switch photocurrent I_{ph} from output D1 to output D2. If current I_M is a sine wave, process is a *demodulation* of the detected signal (wow!)



M1, M2: modulation electrodes, D1, D2: collection electrodes of the photo-demodulator detector (PDD)

features of PDD

advantages:

- High demodulation efficiency
- Fully Compatible with standard CMOS technology

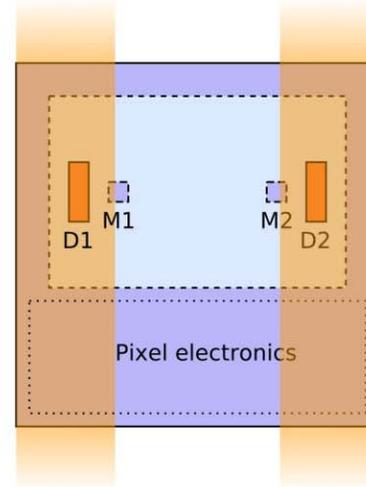
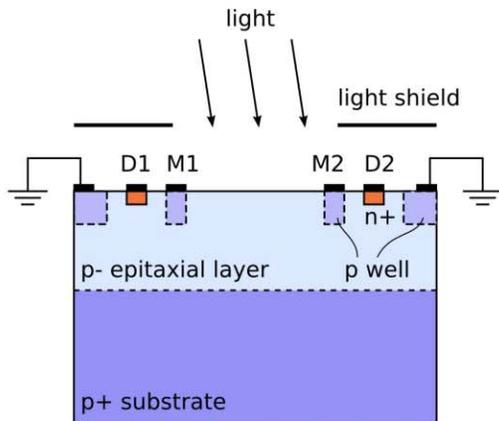


issues:

- High power consumption due to modulation current (about 100 mW)
- Pixel scalability questionable

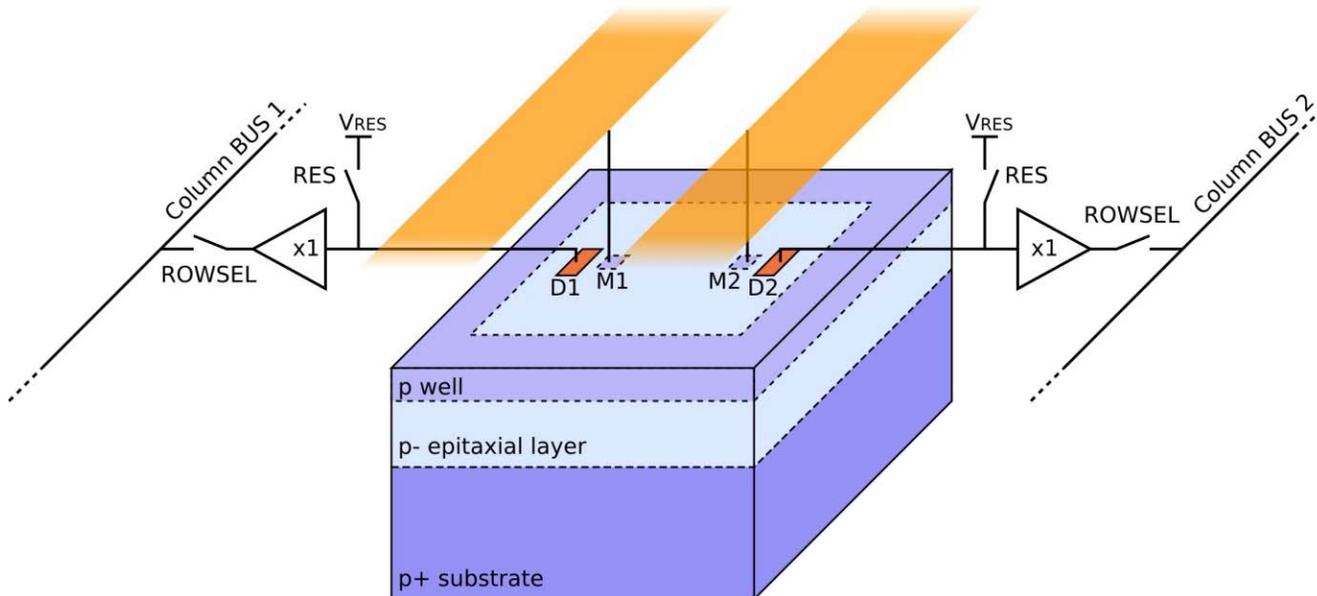


Pixel Architecture

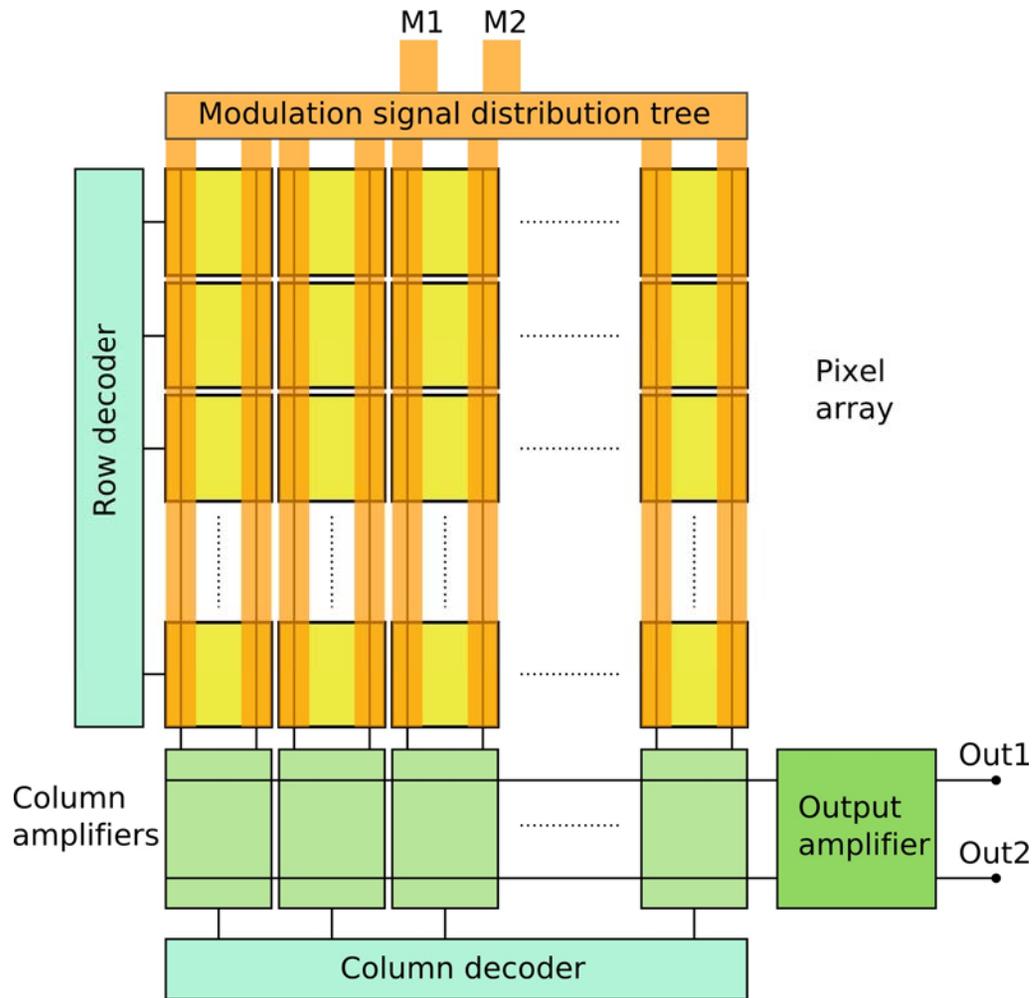


Technology:
180-nm CMOS
Pixel pitch: $10\mu\text{m}$
Fill factor: 24%
1.8-V transistors

Metal shield and modulation signal distribution

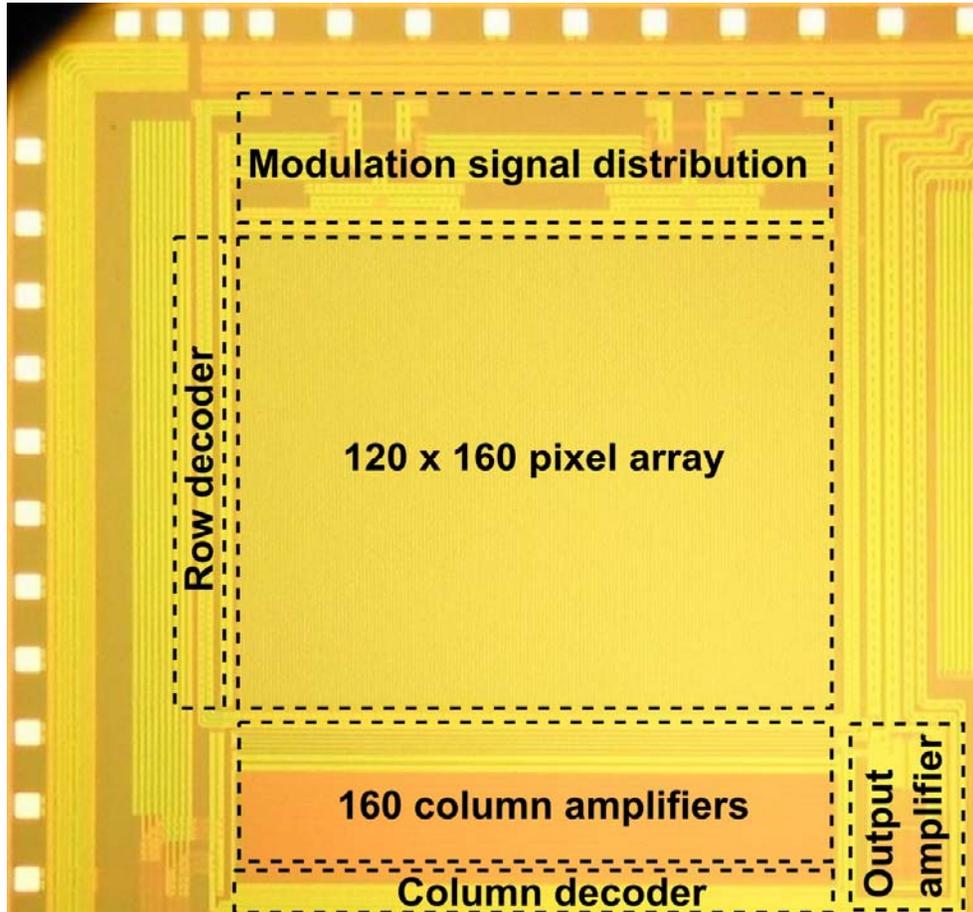


Sensor Architecture



- 120x160 pixel array
- Pseudo-differential pixel
- Column amplifiers
- Output DDS amplifier

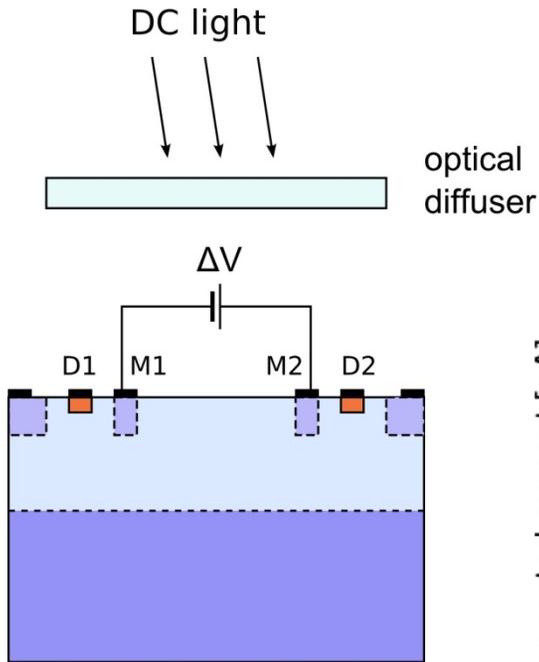
Sensor Chip



- CMOS 0.18 μm 1P4M process
- Sensor area: **2.5x2.5mm²**
- 1.8V and 3.3V transistors
- Epitaxial layer
resistivity: 20 Ohm-cm
thickness: 4 μm

-
- Experimental Results:
 - Photo-detector performance
 - 3D imaging system
-

Photo-demodulator: DC Performance



$R_{\text{MOD}} = 25 \text{ k}\Omega$
dissipation $10 \mu\text{W}$

**DC demodulation
contrast:**

$$\chi = \frac{(I_{D1} - I_{D2})}{(I_{D1} + I_{D2})}$$

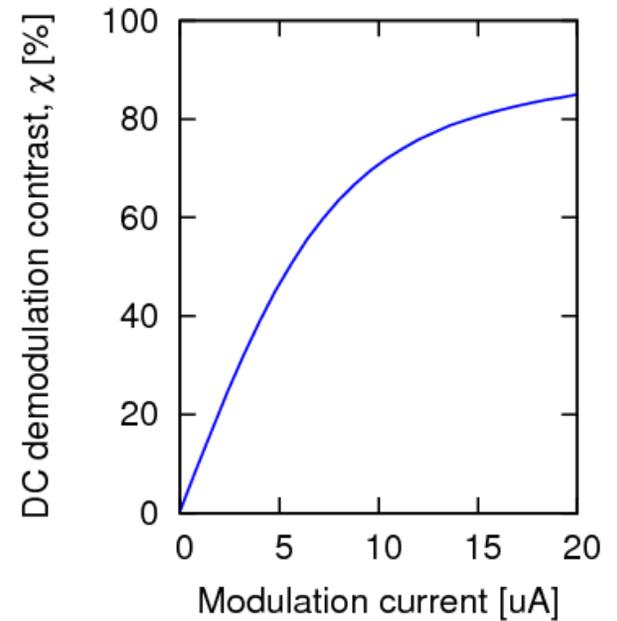
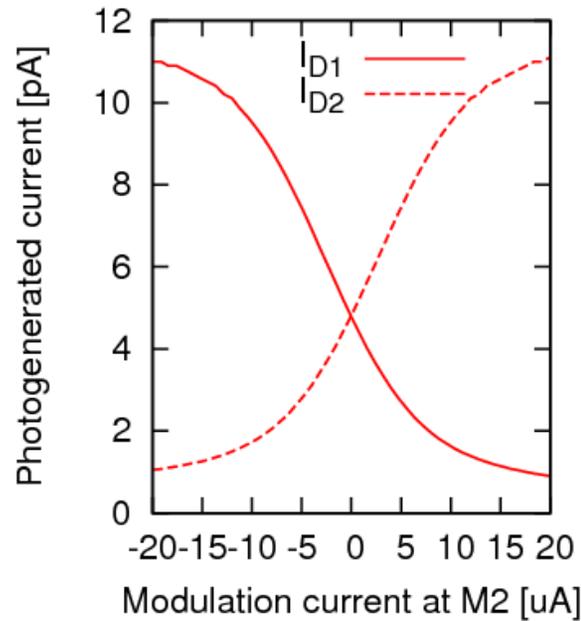
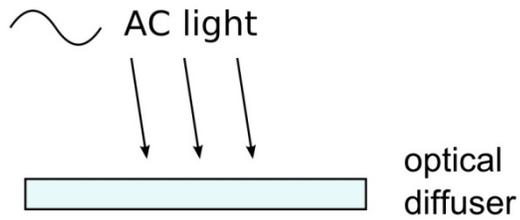


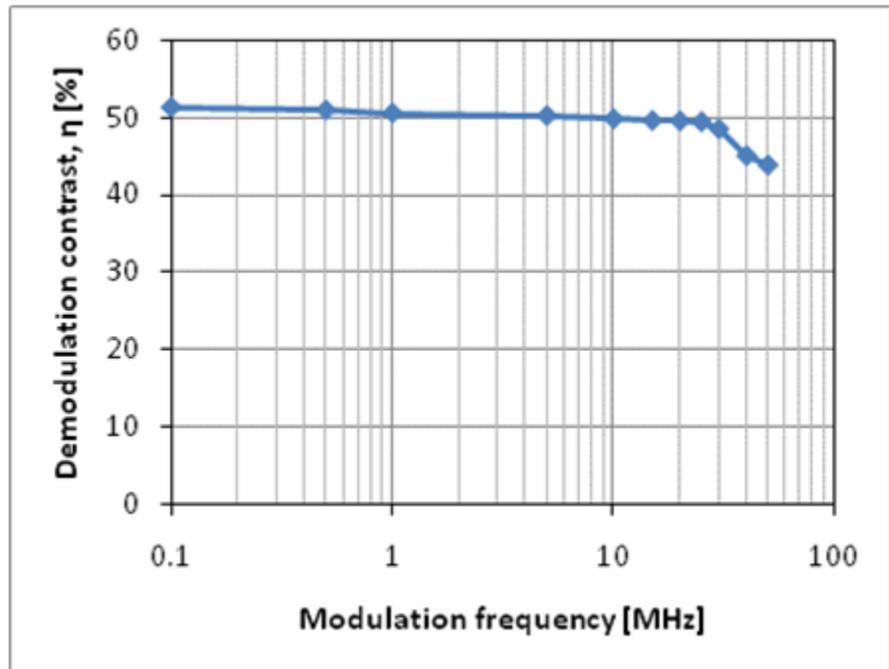
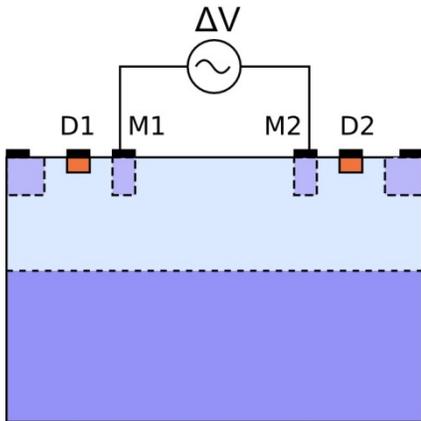
Photo-demodulator: AC Performance



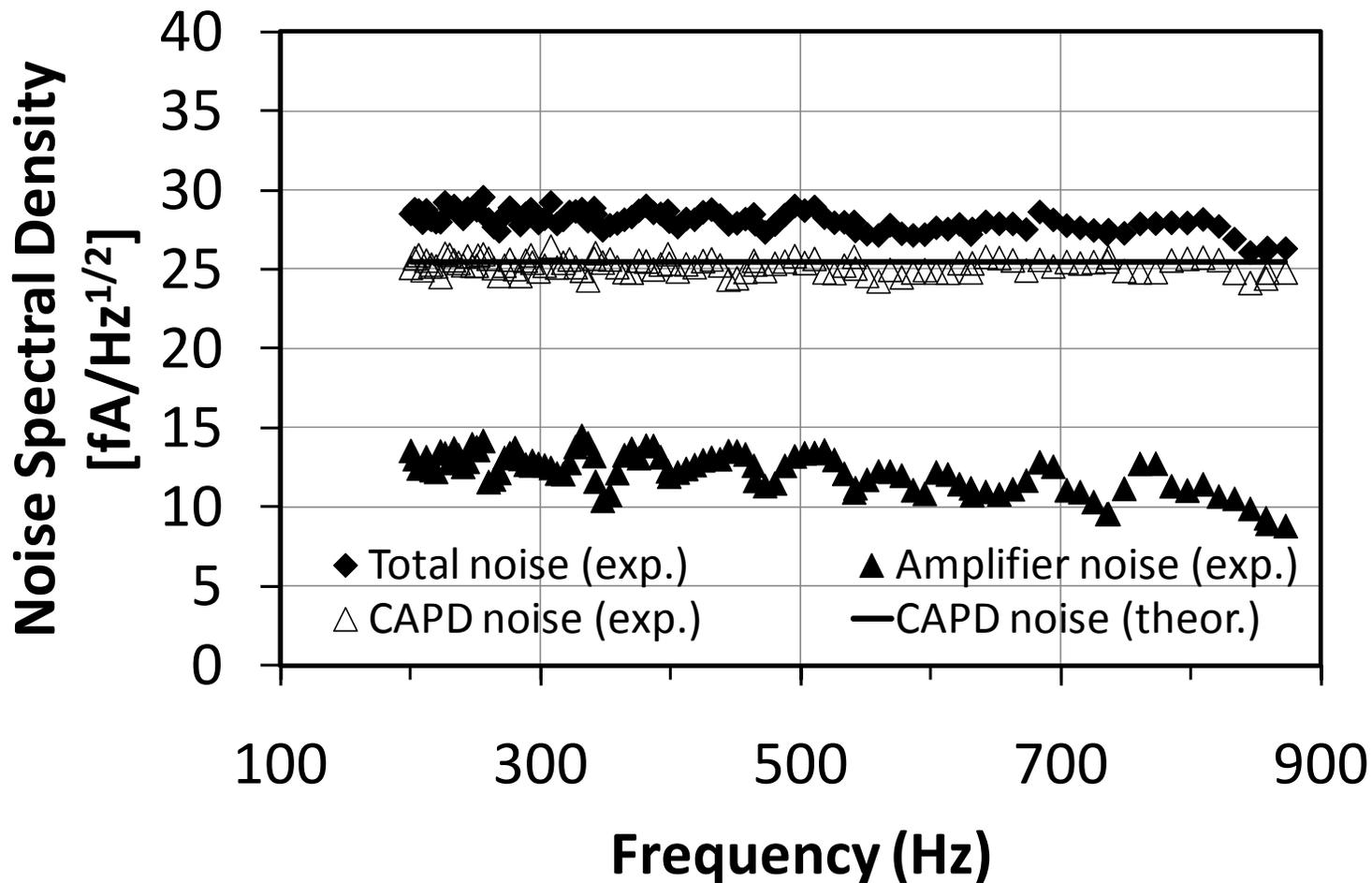
AC demodulation contrast:

$$\chi = \frac{(I_{D1} - I_{D2})_{\max}}{(I_{D1} + I_{D2})}$$

Modulation current: 16 $\mu\text{A}/\text{pixel}$ (peak)



Noise Performance



No appreciable excess noise is observed with respect to the shot-noise level ($I_{c1} \approx 2 \text{ nA}$) due to the modulation resistance

3-D Imaging System



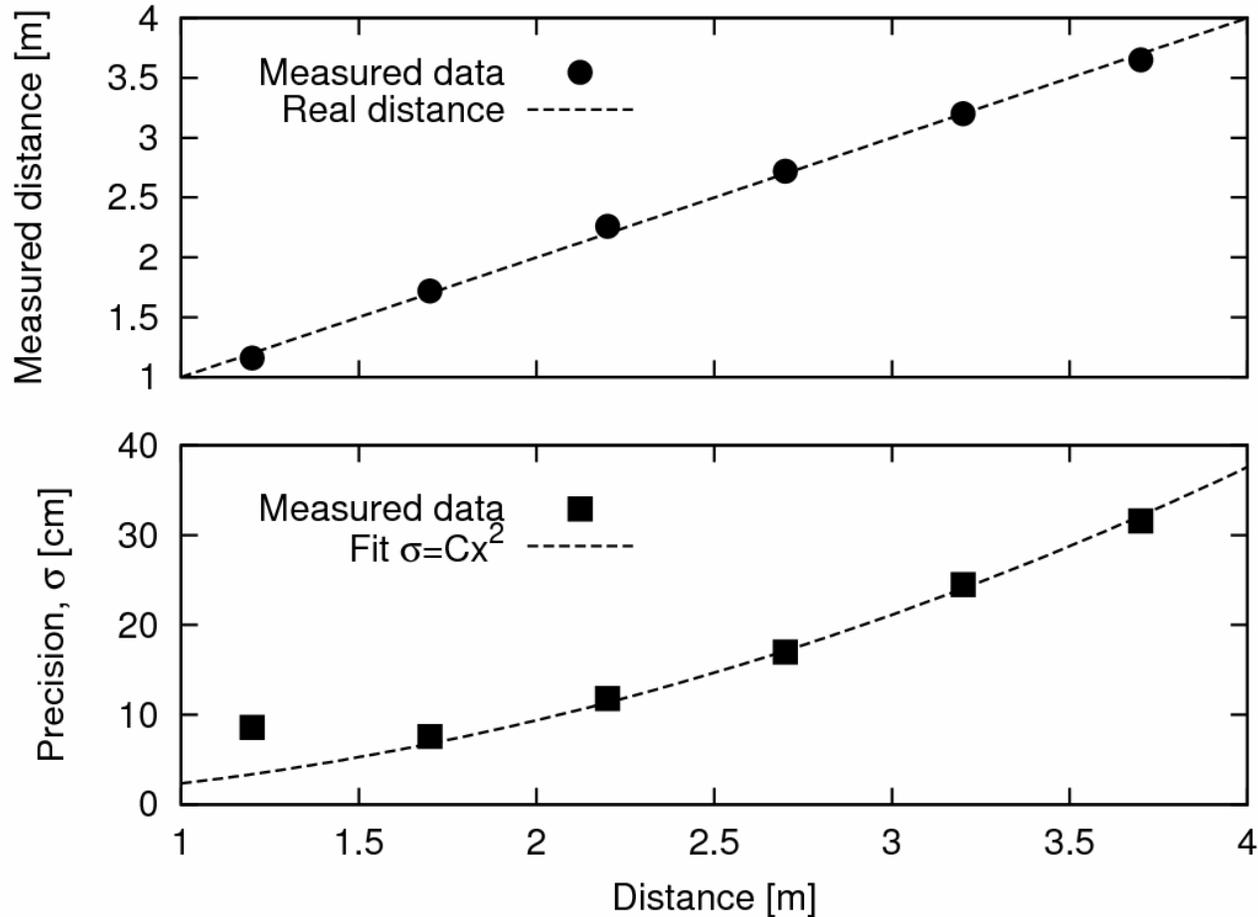
Illumination module:

- source: LED, 20 MHz, λ : 850nm
- power in the FoV: 140 mW
- class (IEC 60825-1): 1M

Sensor:

- objective 2.9-mm, F/1
- sensor FoV $23^\circ \times 30^\circ$
- total modulation current: 400 mA (peak)

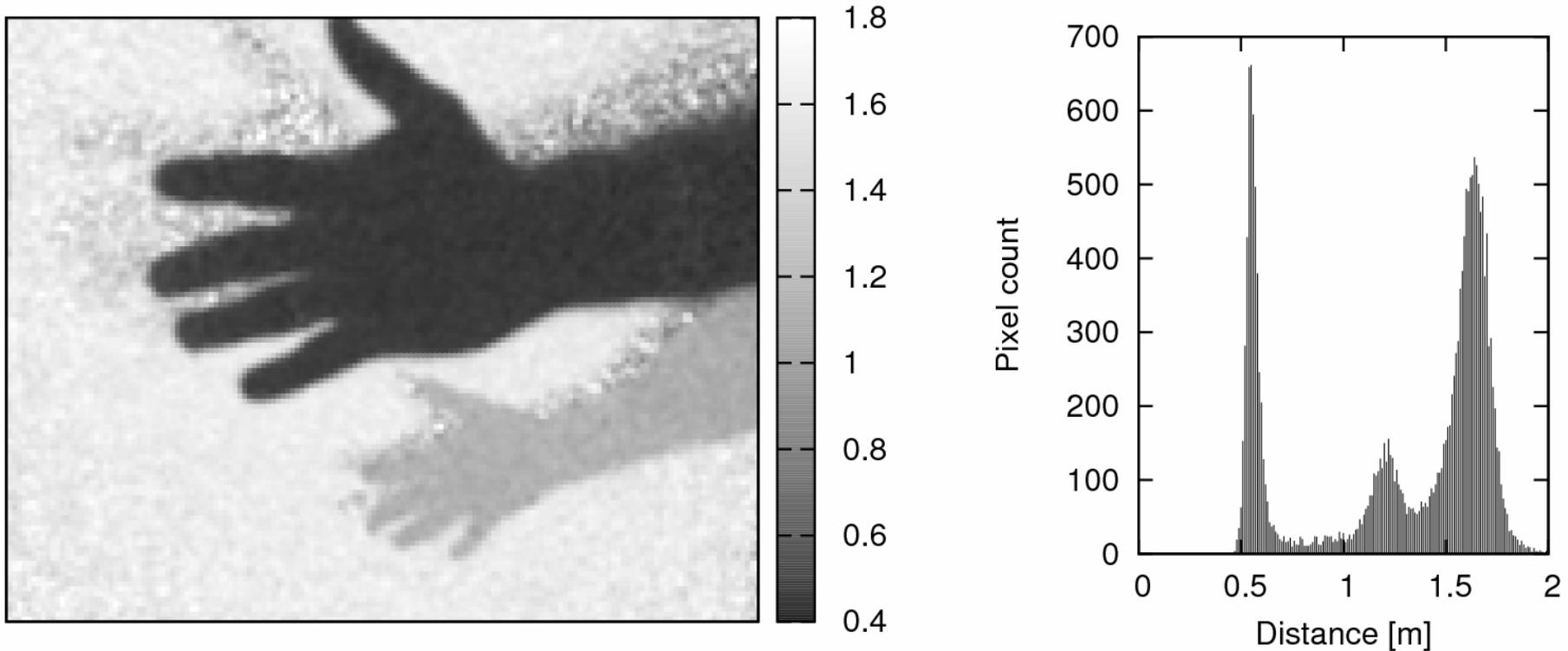
Distance Measurement



Maximum non-linearity: 0.3%

Distance non uniformity among pixels: 0.2cm

3-D Image Example



Acquired with 400ms exposure time, 100 lux ambient light

in conclusion...

- Current Assisted Photo-Demodulator-Detector in CMOS technology demonstrated
 - 10- μm , 24% fill-factor pixel achieved,
 - 50% demodulation contrast at 20MHz and
 - >50MHz cutoff frequency
 - 120x160 3-D image sensor designed
 - real-time 3-D Imaging demonstrated,
 - then...
- ...the SWM CMOS 3-D approach is viable !....

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謝謝

thank you